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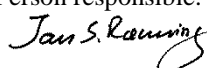
Report no.: 2013.044		ISSN 0800-3416	Grading: Open
Title: Helicopter-borne magnetic, electromagnetic and radiometric geophysical survey in at Langøya in Vesterålen, Nordland			
Authors: Alexei Rodionov, Frode Ofstad, Alexandros Stampolidis & Georgios Tassis.		Client: NGU	
County: Nordland		Municipalities: Bø, Hadsel, Sortland and Øksnes	
Map-sheet name (M=1:250.000) SVOLVÆR		Map-sheet no. and -name (M=1:50.000) 1132 I Nykvåg, 1132 II Stokmarknes, 1132 III Skarvågen, 1232 III Sortland, 1232IV Gavlfjotd	
Deposit name and grid-reference: Sortland UTM 33W 516500 - 762100		Number of pages: 26 Price (NOK): 120,- Map enclosures:	
Fieldwork carried out: July - August 2013	Date of report: September 22 nd 2013	Project no.: 342900	Person responsible: 
Summary: <p>NGU conducted an airborne geophysical survey in Langøya area in July - August 2013 as a part of the MINN project. This report describes and documents the acquisition, processing and visualization of recorded datasets. The geophysical survey results reported herein are 5650 line km, covering an area of 1050 km².</p> <p>The NGU modified Geotech Ltd. Hummingbird frequency domain system supplemented by optically pumped Cesium magnetometer and 1024 channels RSX-5 spectrometer was used for data acquisition.</p> <p>The survey was flown with 200 m line spacing, line direction 135° (North West to South East) in the eastern part and 90° (West to East) in the western part of the survey area, and average speed 80 km/h. The average terrain clearance of the bird was 55 m.</p> <p>Collected data were processed by Alexei Rodionov (AR Geoconsulting, Canada) using Geosoft Oasis Montaj software. Raw total magnetic field data were corrected for diurnal variation and levelled using standard micro levelling algorithm. EM data were filtered and levelled using both automated and manual levelling procedure. Apparent resistivity was calculated from in-phase and quadrature data for all frequencies except for 880 Hz Coplanar coils using a homogeneous half space model. Apparent resistivity for 880 Hz was calculated from quadrature component. All apparent resistivity dataset was filtered using 3x3 convolution filter (high frequencies) or a Butterworth filter (high frequencies). Radiometric data were processed using standard procedures recommended by International Atomic Energy Association.</p> <p>All data were gridded with the cell size of 50 x 50 m and presented as a shaded relief maps at the scale of 1:25 000.</p>			
Keywords: Geophysics		Airborne	Magnetic
Electromagnetic		Gamma spectrometry	Radiometric
			Technical report

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1. INTRODUCTION

Recognising the impact that investment in mineral exploration and mining can have on the socio-economic situation of a region, the government of Norway initiated the MINN program (Mineral resources in North Norway). The goal of this program is to enhance the geological information that is relevant to an assessment of the mineral potential of the three northernmost counties. The airborne geophysical surveys - helicopter borne and fixed wing- are important integral part of MINN program. The airborne survey results reported herein amount to 5650 line km flown (1050 km²) over the Langøya survey area, as shown in Figure 1.

The objective of the airborne geophysical survey was to obtain a dense high-resolution aeromagnetic, electromagnetic and radiometric data over the survey area. This data is required for the enhancement of a general understanding of the regional geology of the area. In this regard, the data can also be used to map contacts and structural features within the property. It also improves defining the potential of known zones of mineralization, their geological settings, and identifying new areas of interest.

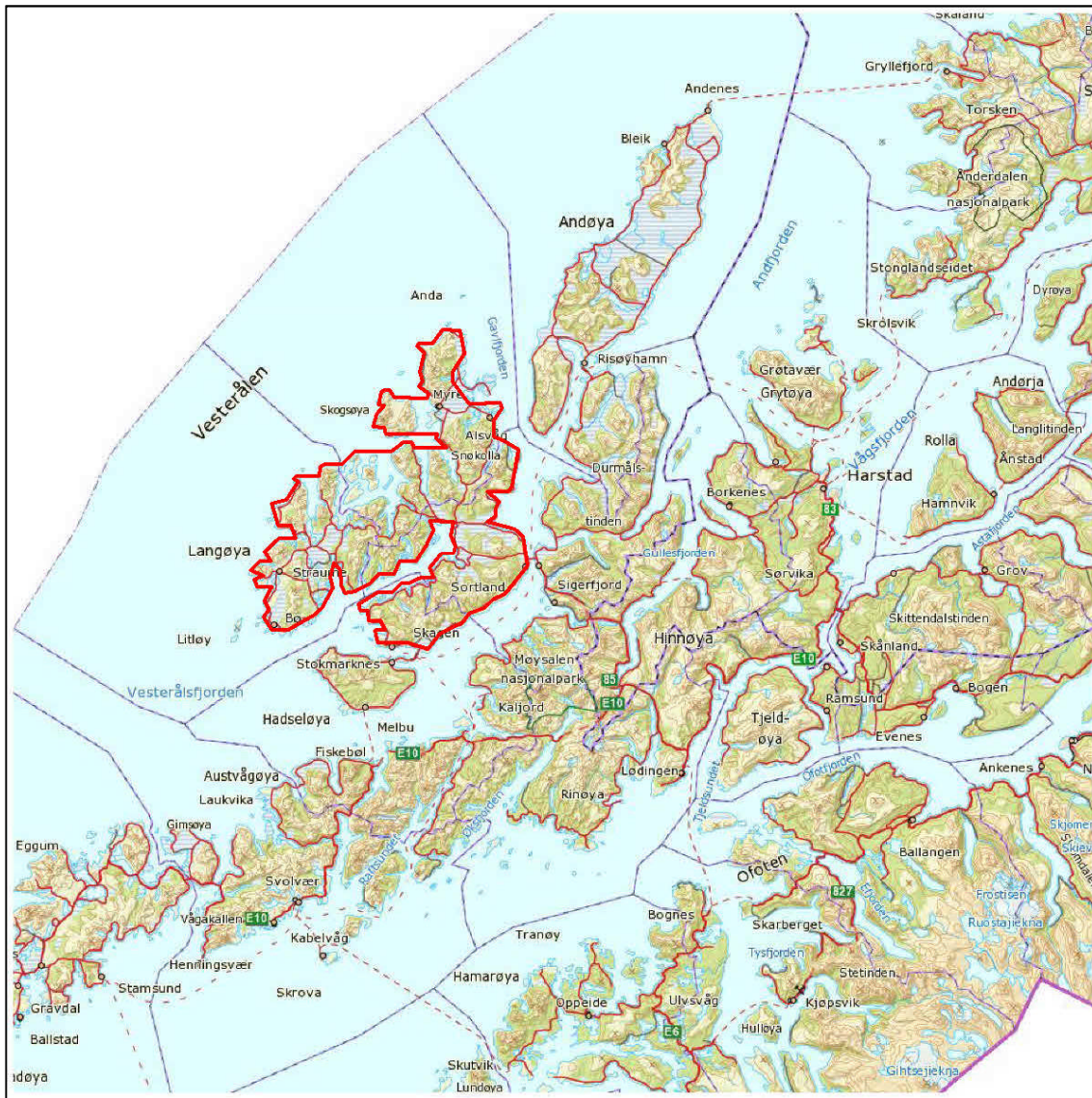


Figure 1: Langøya survey area

The survey incorporated the use of a Hummingbird™ five-frequency electromagnetic system supplemented by a high-sensitivity caesium magnetometer, gamma-ray spectrometer and radar altimeter. A GPS navigation computer system with flight path indicators ensured accurate positioning of the geophysical data with respect to the World Geodetic System 1984 geodetic datum (WGS-84).

2. LOCATION

Langøya is a part of Vesterålen archipelago and is situated in Nordland county. The island includes the municipalities of Bø and Øksnes as well as parts of the municipalities of Sortland and Hadsel.

3. SURVEY SPECIFICATIONS

3.1 Airborne Survey Parameters

NGU used a modified Hummingbird™ electromagnetic and magnetic helicopter survey system designed to obtain low level, slow speed, detailed airborne magnetic and electromagnetic data (Geotech 1997). The system was supplemented by 1024 channel gamma-ray spectrometer which was used to map ground concentrations of U, Th and K.

The airborne survey began on July 16th and ended on August 5th, 2013. A Eurocopter AS350-B3 helicopter from helicopter company HeliScan AS was used to tow the bird. The survey lines were spaced 200 m apart. Lines were oriented at a 135° azimuth in eastern part and at 90° in western part of the survey area in UTM zone 33W coordinates.

The magnetic and electromagnetic sensors are housed in a single 7.5 m long bird, which was maintained at an average of 55 m above the topographic surface. A gamma-ray spectrometer, installed under the belly of the helicopter, registered natural gamma ray radiation simultaneously with the acquisition of magnetic/EM data.

Rugged terrain and abrupt changes in topography may affect the aircraft pilot's ability to 'drape' the terrain; therefore there are positive and negative variations in sensor height with respect to the standard height, which is defined as 30 m plus a height of obstacles (trees, power lines etc.).

The ground speed of the aircraft varied from 50 – 110 km/h depending on topography, wind direction and its magnitude. On average the ground speed during measurements is calculated to 75 km/h. Magnetic data were recorded at 0.2 second intervals resulting in approximately 4 m point spacing. EM data were recorded at 0.1 second intervals resulting in data with a sample increment of 2.0 m along the ground in average. Spectrometry data were recorded every 1 second giving a point spacing of approximately 21 meter. The above parameters were designed to allow for sufficient detail in the data to detect subtle anomalies that may represent mineralization and/or rocks of different lithological and petrophysical composition.

Navigation system uses GPS/GLONASS satellite tracking systems to provide real-time WGS-84 coordinate locations for every second. The accuracy achieved with no differential

corrections is reported to be ± 5 m in the horizontal directions. The GPS receiver antenna was mounted externally to the tail tip of the helicopter.

For quality control, the electromagnetic, magnetic and radiometric, altitude and navigation data were monitored on four separate windows in the operator's display during flight while they were recorded in three data ASCII streams to the PC hard disk drive.

3.2 Airborne Survey Instrumentation

Instrument specification is given in table 1. Frequencies and coil configuration for the Hummingbird EM system is given in table 2.

Table 1. Instrument Specifications

Instrument	Producer/Model	Accuracy	Sampling Frequency/Interval
Magnetometer	Scintrex Cs-2	0,002 nT	5 Hz
Base magnetometer	GEM GSM-19	0.1 nT	3 sec
Electromagnetic	Geotech Hummingbird	1 – 2 ppm	10 Hz
Gamma spectrometer	Radiation Solutions RSX-5	1024 ch's, 16 liters down, 4 liters up	1 Hz
Radar altimeter	Bendix/King KRA 405B	$\pm 3\%$ 0 – 500 fot $\pm 5\%$ 500 – 2500 fot	1 Hz
Pressure/temperature	Honeywell PPT	$\pm 0,03\%$ FS	1 Hz
Navigation	Topcon GPS-receiver	± 5 meter	1 Hz
Acquisition system	NGU custom build software		

Table 2. Hummingbird electromagnetic system, frequency and coil configurations

Coils:	Frequency	Orientation	Separation
A	7700 Hz	Coaxial	6.20 m
B	6600 Hz	Coplanar	6.20 m
C	980 Hz	Coaxial	6.025 m
D	880 Hz	Coplanar	6.025 m
E	34000 Hz	Coplanar	4.87 m

The electromagnetic, magnetic and radiometric, altitude and navigation data were monitored on the operator's displays during flight while they were recorded to the PC hard disk drive. Spectrometry data were also recorded to internal hard drive of the spectrometer. The data files were transferred to the field workstation via USB flash drive. The raw data files were backed up onto USB flash drive in the field.

3.3 Airborne Survey Logistics Summary

Traverse (survey) line spacing:	200 metres
Traverse line direction:	135° NW –SE, Eastern part 90° W-E, Western part
Nominal aircraft ground speed:	50 - 110 km/h
Average sensor terrain clearance EM+Mag:	55 metres
Average sensor terrain clearance Rad:	85 metres
Sampling rates:	0.2 seconds - magnetometer 0.1 seconds - electromagnetics 1.0 second - spectrometer, GPS, altimeter

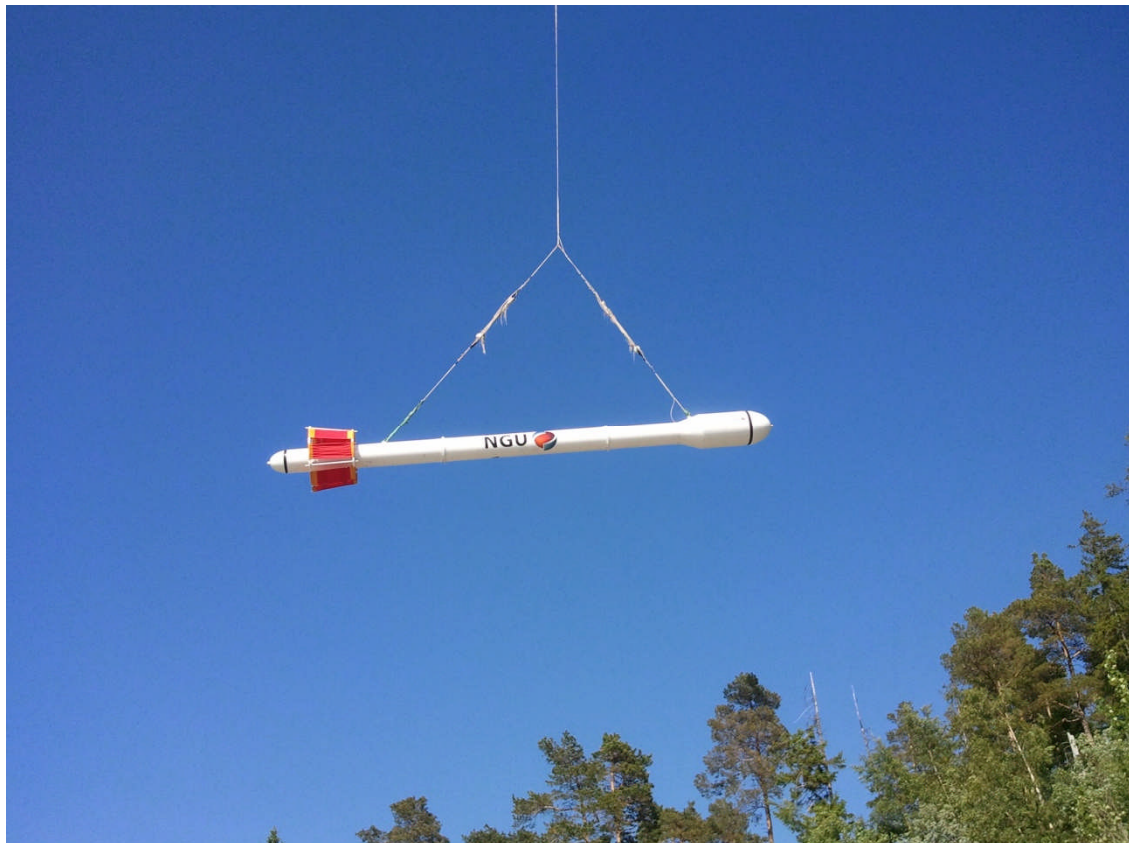


Figure 2: Hummingbird system in air

4. DATA PROCESSING AND PRESENTATION

All data were processed by Alexei Rodionov (AR Geoconsulting Ltd., Canada) in Calgary. The ASCII data files were loaded into three separate Oasis Montaj databases. All three datasets were processed consequently according to processing flow charts shown in Appendix A1, A2 and A3.

4.1 Total Field Magnetic Data

At the first stage the magnetic data were visually inspected and spikes were removed manually. Non-linear filter was also applied to airborne raw data to eliminate short-period spikes. Then the data from basemag station were imported in magnetic database using the standard Oasis magbase.gx module. Diurnal variation channel was also inspected for spikes

and spikes were removed manually if necessary. Typically, several corrections have to be applied to magnetic data before gridding - heading correction, lag correction and diurnal correction.

Diurnal Corrections

The temporal fluctuations in the magnetic field of the earth affect the total magnetic field readings recorded during the airborne survey. This is commonly referred to as the magnetic diurnal variation. These fluctuations can be effectively removed from the airborne magnetic dataset by using a stationary reference magnetometer that records the magnetic field of the earth simultaneously with the airborne sensor. Magnetic diurnals were within the standard NGU specifications during the entire survey (Rønning 2013).

The base magnetometer was located at Holansneset (UTM 510600 – 7613500) for the first two flights and Sørneset (UTM 515000 – 7617000) for the rest. Both location lies at the eastern edge of the survey area. Diurnal variations were measured with GEM GSM-19 magnetometer. The average magnetic field was 52718 nT. The base station computer clock was synchronized with the DAS clock on a daily basis. The recorded data are merged with the airborne data and the diurnal correction is applied according to equation (1).

$$\mathbf{B}_{Tc} = \mathbf{B}_T + (\bar{\mathbf{B}}_B - \mathbf{B}_B), \quad (1)$$

Where:

\mathbf{B}_{Tc} = Corrected airborne total field readings

\mathbf{B}_T = Airborne total field readings

$\bar{\mathbf{B}}_B$ = Average datum base level

\mathbf{B}_B = Base station readings

Corrections for Lag and heading

Neither a lag nor cloverleaf tests were performed before the survey. According to previous reports the lag between logged magnetic data and the corresponding navigational data was 1-2 fids. Translated to a distance it would be no more than 10 m - the value comparable with the precision of GPS. A heading error for a towed system is usually either very small or non-existent. So no lag and heading corrections were applied.

Magnetic data gridding and presentation

Before gridding, flight data were split by lines. For the purposes of data presentation and interpretation the total field magnetic data are gridded with a cell size of 50 m, which represents one quarter of the 200 m average line spacing. A micro levelling technique was applied to the magnetic data to remove small line-to-line levelling errors and a 3 x 3 convolution filter was passed over the final grid to smooth the grid image.

The Vertical Gradient (VG) and the Tilt Derivative (TD) of the total magnetic field was calculated from the resulting total magnetic field map. These signals transform the shape of the magnetic anomaly from any magnetic inclination to positive body-centred anomaly and it's widely utilized for mapping of structures.

4.2 Electromagnetic Data

The DAS computer records both an in-phase and a quadrature value for each of the five coil sets of the electromagnetic system. Instrumental noise and drift should be removed before computation of an apparent resistivity.

Instrumental noise

In-phase and quadrature data were filtered with 3 fids non-linear filter to eliminate spheric spikes which were represented as irregular spikes of large amplitude in records. Simultaneously, the 30 fids low-pass filter was also applied to suppress high frequency components of instrumental and cultural noise. Cultural noise was relatively low within the survey area and observed occasionally on 980 and 880 Hz at the intersection with power lines. Cultural noise, visible at some lines on 34000 Hz, is probably attributed to radio transmitters and/or bird swaying. Generally, cultural noise did not affected EM data significantly.

Instrument Drift

In order to remove the effects of instrument drift caused by gradual temperature variations in the transmitting and receiving circuits, background responses are recorded during each flight. To obtain a background level the bird is raised to an altitude of approximately 1200 ft above the topographic surface so that no electromagnetic responses from the ground are present in the recorded traces. The EM traces observed at this altitude correspond to a background (zero) level of the system. If these background levels are recorded at 20-30 minute intervals, then the drift of the system (assumed to be linear) can be removed from the data by resetting these points to the initial zero level of the system. The drift must be removed on a flight-by-flight basis, before any further processing is carried out. Geosoft HEM module was used for applying drift correction. Residual instrumental drift, usually small, but often non-linear, was manually removed on line-to-line basis. During flights 1, 2, 6, 8-12, 15, 16, 19, 25 and 29, instrumental drift on 880 Hz coplanar in phase channel was strongly non-linear most of the time. Non-linearity was also observed on other EM channels but in lesser degree.

Apparent resistivity calculation and presentation

When levelling of the EM data was complete, apparent resistivity was calculated from in-phase and quadrature EM components using a homogeneous half space model of the Earth (Geosoft HEM module) for four frequencies. Apparent resistivity for 880Hz was calculated from quadrature component only, because inphase component could not be levelled correctly due to strong non-linear drift. Threshold of 1 ppm was set for inversion for all frequencies.

Secondary electromagnetic field decays rapidly with the distance (height of the sensors) – as $z^{-2} - z^{-5}$ depending on the shape of the conductors and, at certain height, signals from the ground sources become comparable with instrumental noise. Levelling errors or precision of levelling can lead sometimes to appearance of artificial resistivity anomalies when data were collected at high instrumental altitude. Application of threshold allows excluding such data from an apparent resistivity calculation, though not completely. It's particularly noticeable in low frequencies datasets. Data, recorded at the height above 100 m were considered as non-reliable and removed. Remaining resistivity data were visually inspected; artificial anomalies associated with high altitude measurements were manually removed and then levelled. Revised resistivity data were gridded with a cell size 50 m and 3x3 convolution filter was applied to smooth the resistivity grids for 34000, 6600, 7000 Hz. Batterworth filter was applied to smooth the resistivity grids for 880 and 980 Hz.

4.3 Radiometric data

In processing of the airborne gamma ray spectrometry data, live time corrected U, Th and K were corrected for the aircraft and cosmic background (e.g. Grasty et al. 1991; IAEA 2003). The upward detector method, as discussed in IAEA (2003), was applied to remove the effects of radon in the air below and around the helicopter. Window stripping was used to isolate count rates from the individual radio-nuclides K, U and Th (IAEA, 2003). The topography in the region was rough, and the sensor was not always at a constant altitude. Stripped window counts were therefore corrected for variations in flying height to a constant height of 60 m. Data, recorded at the height above 150 m were considered as non-reliable and removed from processing. Finally, count rates were converted to effective ground element concentrations using calibration values derived from calibration pads at the Geological Survey of Norway in Trondheim. A list of the parameters used in the processing scheme is given in Appendix A3. For further reading regarding standard processing of airborne radiometric data, we recommend the publication from Minty et al. (1997).

Quality of the radiometric data was within standard NGU specifications (Rønning 2013) except for a few short line segments where data were lost due to lack of GPS-signal.

5. PRODUCTS

Processed digital data from the survey are presented as:

1. Six Geosoft XYZ files:
Langoya_Mag1.xyz, Langoya_EM1.xyz, Langoya_Rad1.xyz, Langoya_Mag2.xyz,
Langoya_EM2.xyz, Langoya_Rad2.xyz,
2. Coloured maps at the scale 1:25000 available from NGU on request.

Table 3: Maps in scale 1:25000 available from NGU on request.

Map #	Name
2013.044-01	Total magnetic field
2013.044-02	Magnetic Vertical Derivative
2013.044-03	Magnetic Tilt Derivative
2013.043-04	Apparent resistivity, Frequency 34000 Hz, coplanar coils
2013.044-05	Apparent resistivity, Frequency 6600 Hz, coplanar coils
2013.044-06	Apparent resistivity, Frequency 880 Hz, coplanar coils
2013.044-07	Apparent resistivity, Frequency 7000 Hz, coaxial coils
2013.044-08	Apparent resistivity, Frequency 9800 Hz, coaxial coils
2013.044-09	Uranium ground concentration
2013.044-10	Thorium ground concentration
2013.044-11	Potassium ground concentration
2013.044-12	Radiometric Ternary Map

Downscaled images of the maps are shown on figures 4 to 15.

6. REFERENCES

- Geotech 1997: Hummingbird Electromagnetic System. User manual. Geotech Ltd. October 1997
- Grasty, R.L., Holman, P.B. & Blanchard 1991: Transportable Calibration pads for ground and airborne Gamma-ray Spectrometers. Geological Survey of Canada. Paper 90-23. 62 pp.
- IAEA 2003: Guidelines for radioelement mapping using gamma ray spectrometry data. IAEA-TECDOC-1363, Vienna, Austria. 173 pp.
- Minty, B.R.S., Luyendyk, A.P.J. and Brodie, R.C. 1997: Calibration and data processing for gamma-ray spectrometry. AGSO – Journal of Australian Geology & Geophysics. 17(2). 51-62.
- Naudy, H. and Dreyer, H. 1968: Non-linear filtering applied to aeromagnetic profiles. Geophysical Prospecting. 16(2). 171-178.
- Rønning, J.S. 2013: NGUs helikoptermålinger. Plan for sikring og kontroll av datakvalitet. NGU Intern rapport 2013.001, (38 sider).

Appendix A1: Flow chart of magnetic processing

Meaning of parameters is described in the referenced literature.

Processing flow:

- Quality control.
- Visual inspection of airborne data and manual spike removal
- Import magbase data to Geosoft database
- Inspection of magbase data and removal of spikes
- Correction of data for diurnal variation
- Splitting flight data by lines
- Gridding
- Microlevelling
- Convolution filter

Appendix A2: Flow chart of EM processing

Meaning of parameters is described in the referenced literature.

Processing flow:

- Filtering of in-phase and quadrature channels with low pass filters
- Automated leveling
- Quality control
- Visual inspection of data.
- Splitting flight data by lines
- Manual removal of remaining part of instrumental drift
- Calculation of an apparent resistivity for each frequency using both - in-phase and quadrature channels (except 880 Hz where resistivity was calculated using quadrature component only)
- Gridding
- Convolution or Batterworth filters

Appendix A3: Flow chart of radiometry processing

Underlined processing stages are not only applied to the K, U and Th window, but also to the total. Meaning of parameters is described in the referenced literature.

Processing flow:

- Quality control
- Airborne and cosmic correction (IAEA, 2003)

Used parameters: (determined by high altitude calibration flights near Seljord in June 2012)

Aircraft background counts:

K window	7
U window	0.9
Th window	0.9
Uup window	0
Total counts	36

Cosmic background counts (normalized to unit counts in the cosmic window):

K window	0.0617
U window	0.0454
Uup window	0.0423
Th window	0.0647
Total counts	1.0379

- Radon correction using upward detector method (IAEA, 2003)
Used parameters (determined from survey data over water and land):

a_u :	0.3196	b_u :	0.5128
a_K :	0.9867	b_K :	1.5687
a_T :	0.0419	b_T :	2772
a_{Tc} :	18.897	b_{Tc} :	0
a_1 :	0.08614	a_2 :	0.00362

- Stripping correction (IAEA, 2003)
Used parameters (determined from measurements on calibrations pads at the NGU on May 6 2013):

a	0.049524
b	-0.00169
g	-0.00131
alpha	0.29698
beta	0.47138
gamma	0.82905

- Height correction to a height of 60 m
Used parameters (determined by high altitude calibration flights near Langoya in July 2013):
Attenuation factors in 1/m:

K:	-0.001634
U:	-0.00777
Th:	-0.0088
Total counts:	-0.01148

- Converting counts at 60 m heights to element concentration on the ground
Used parameters (determined from measurements on calibrations pads at the NGU on May 6 2013):
Sensitivity (elements concentrations per count)::

K:	0.007545 %/counts
U:	0.088909 ppm/counts
Th:	0.151433 ppm/counts

- Microlevelling using Geosoft menu and smoothening by a convolution filtering
Used parameters for microlevelling:

De-corrugation cutoff wavelength:	800 m
Cell size for gridding:	200 m
Naudy (1968) Filter length:	800 m

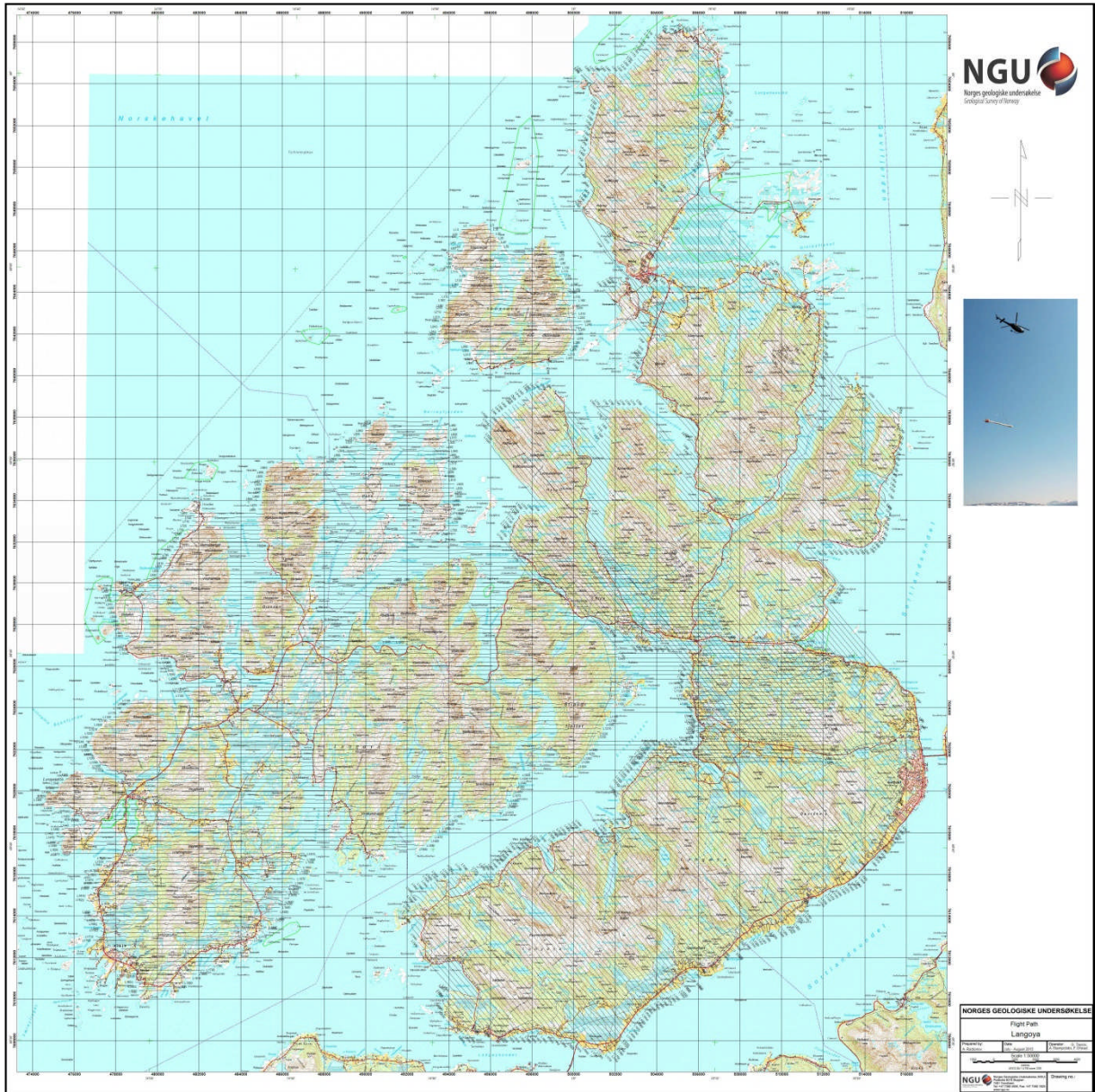


Figure 3: Langoya survey area with flight path.

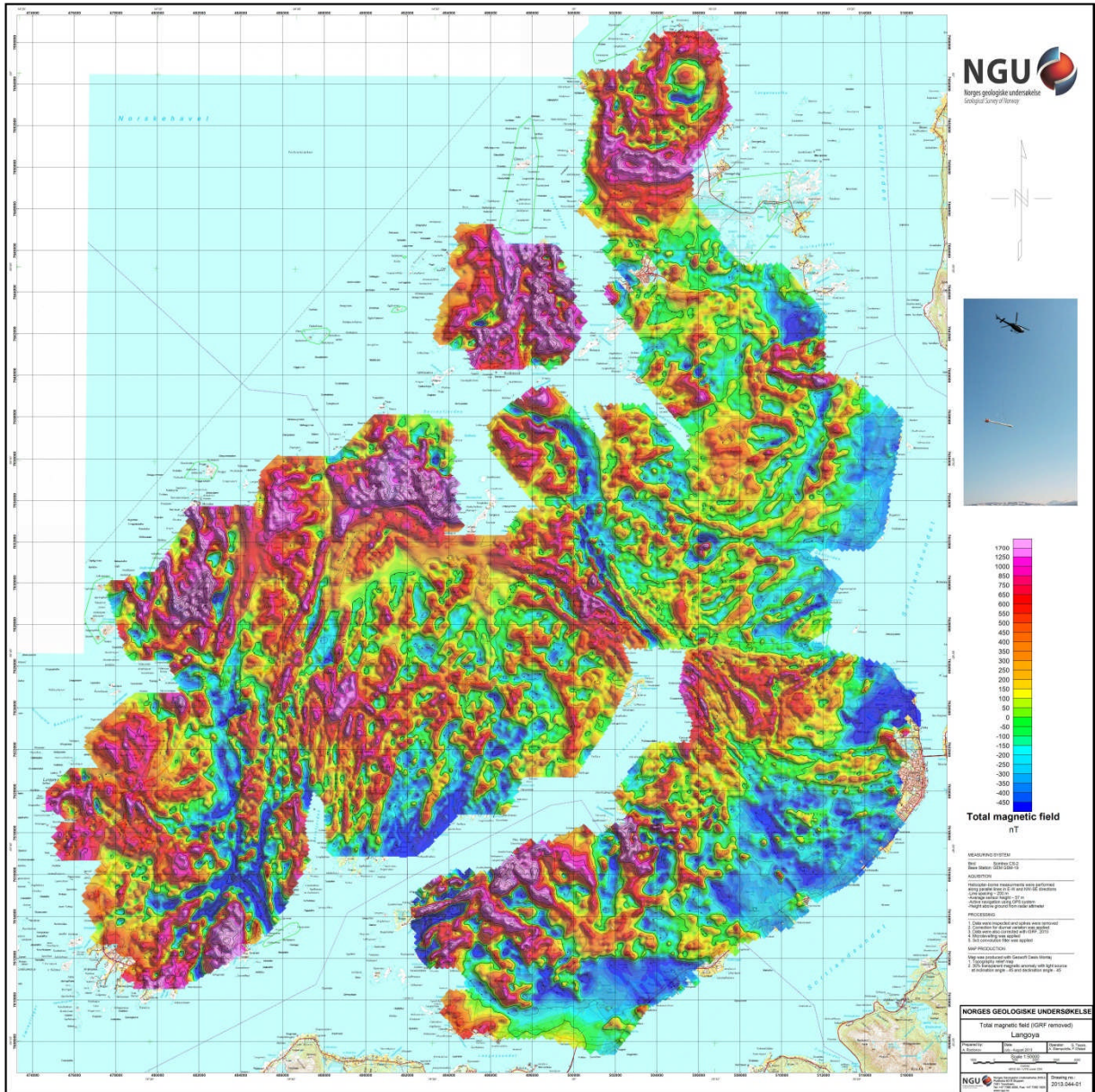


Figure 4: Total Magnetic Field

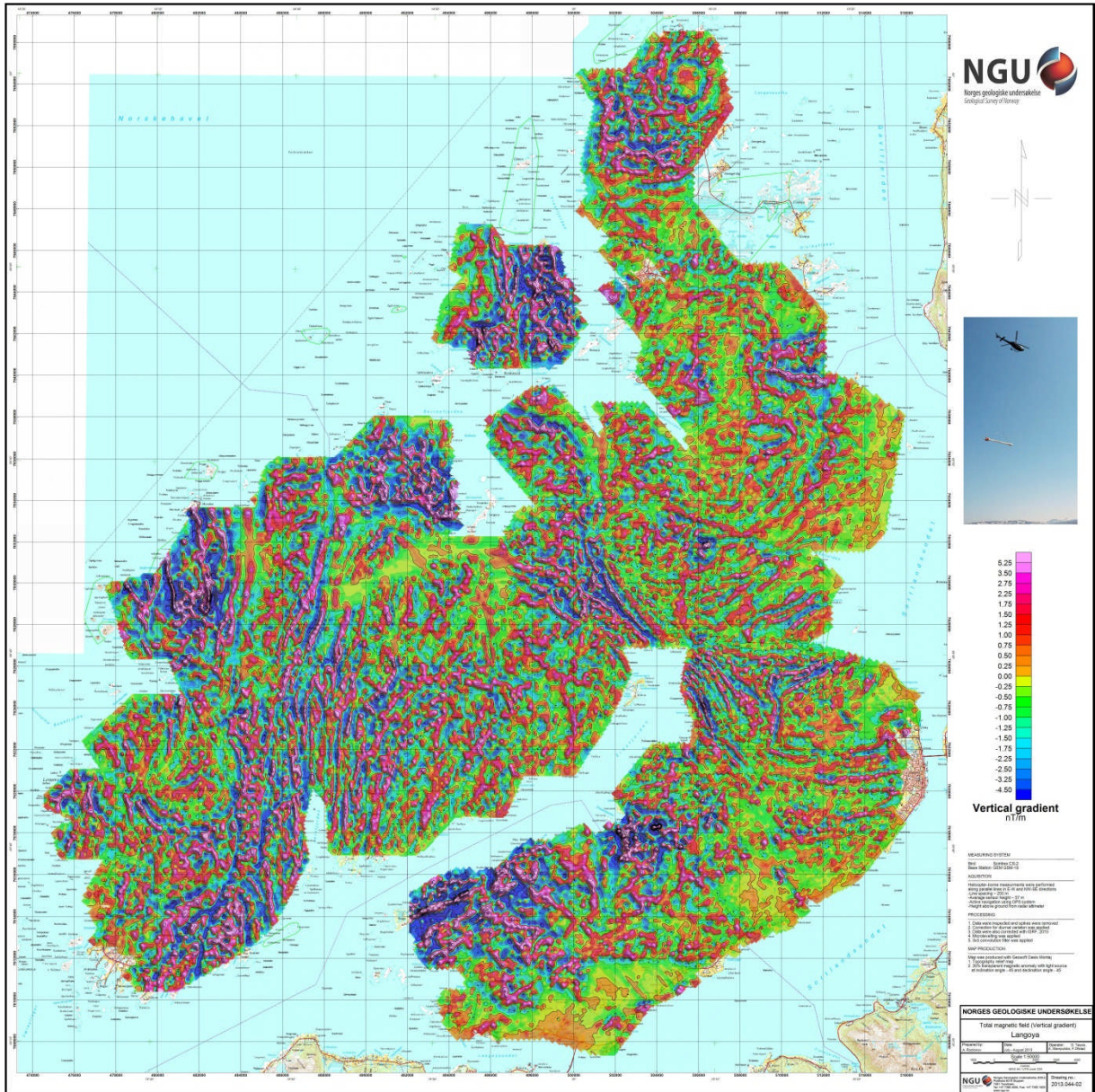


Figure 5: Magnetic Vertical Derivative

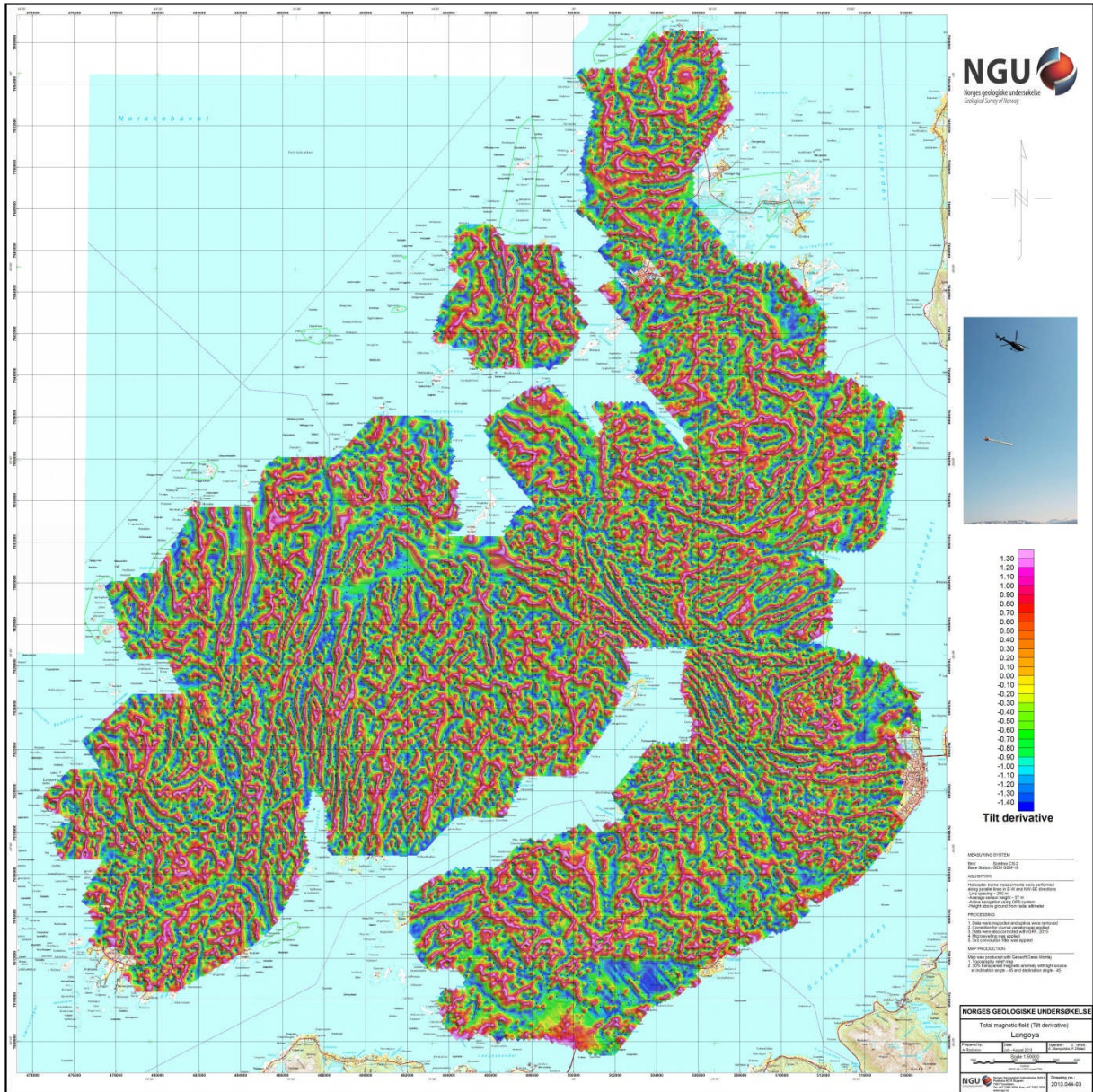


Figure 6: Magnetic Tilt Derivative

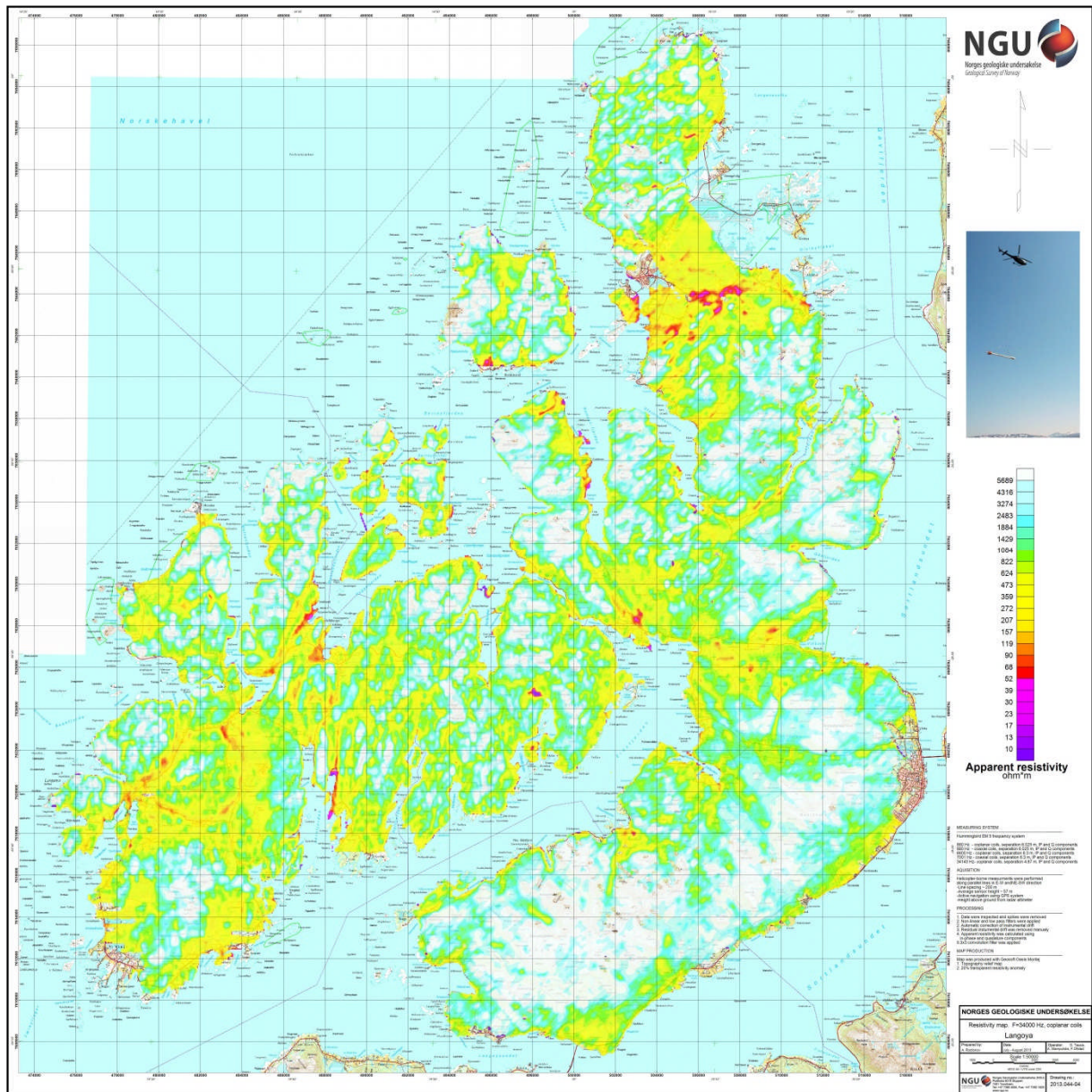


Figure 7: Apparent resistivity. Frequency 34000 Hz, Coplanar coils

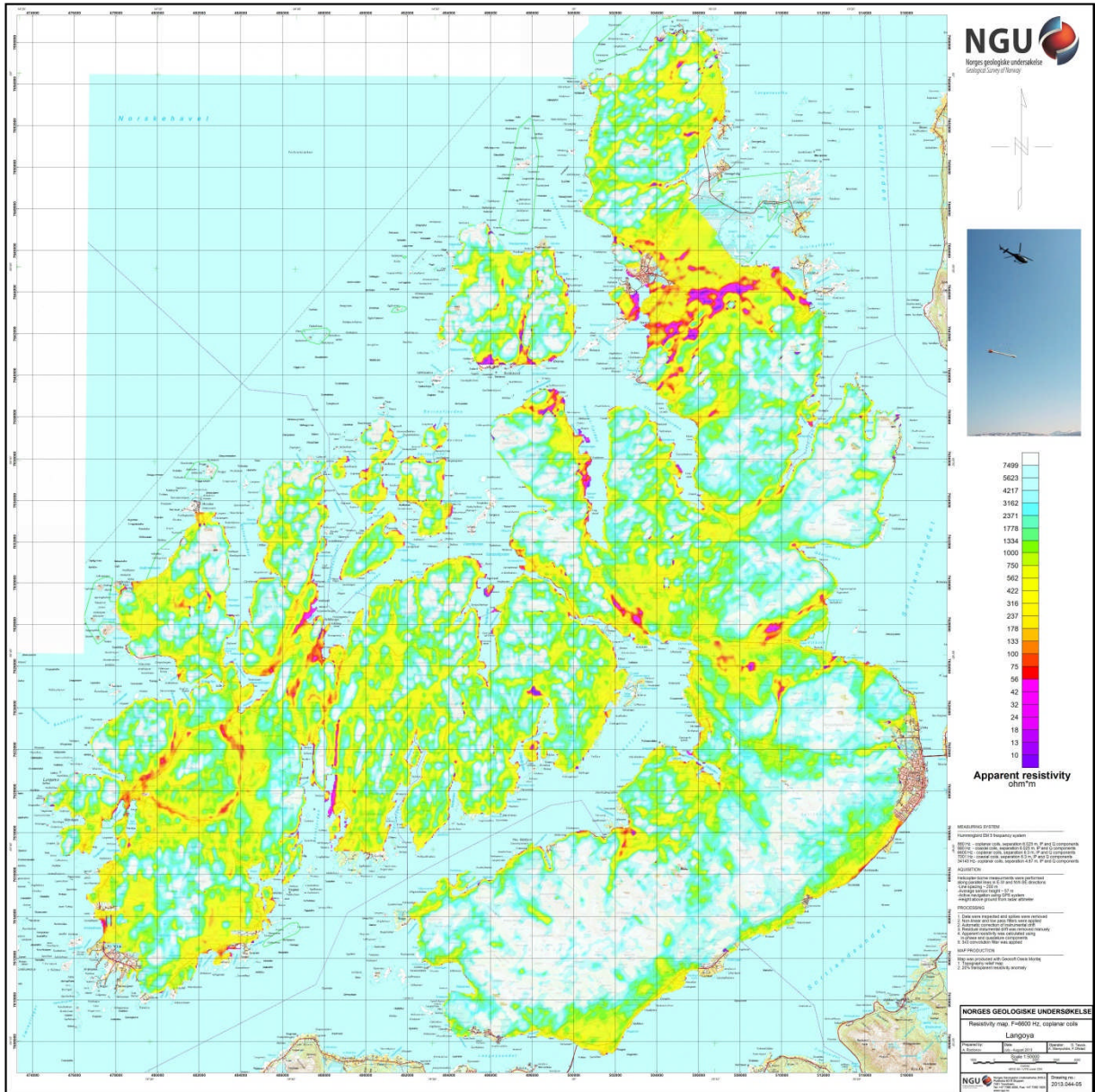


Figure 8: Apparent resistivity. Frequency 6600 Hz, Coplanar coils

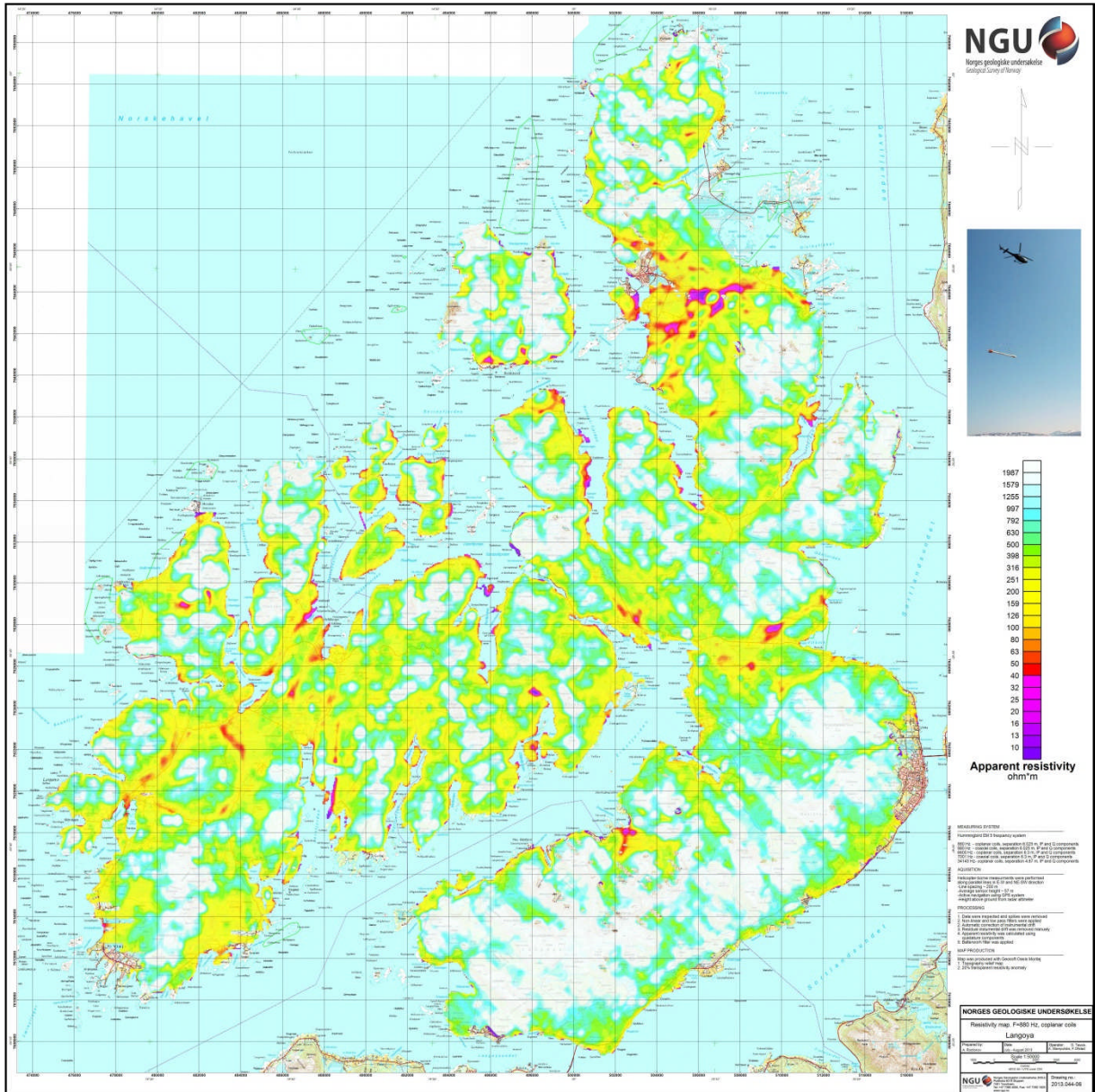


Figure 9: Apparent resistivity. Frequency 880 Hz, Coplanar coils

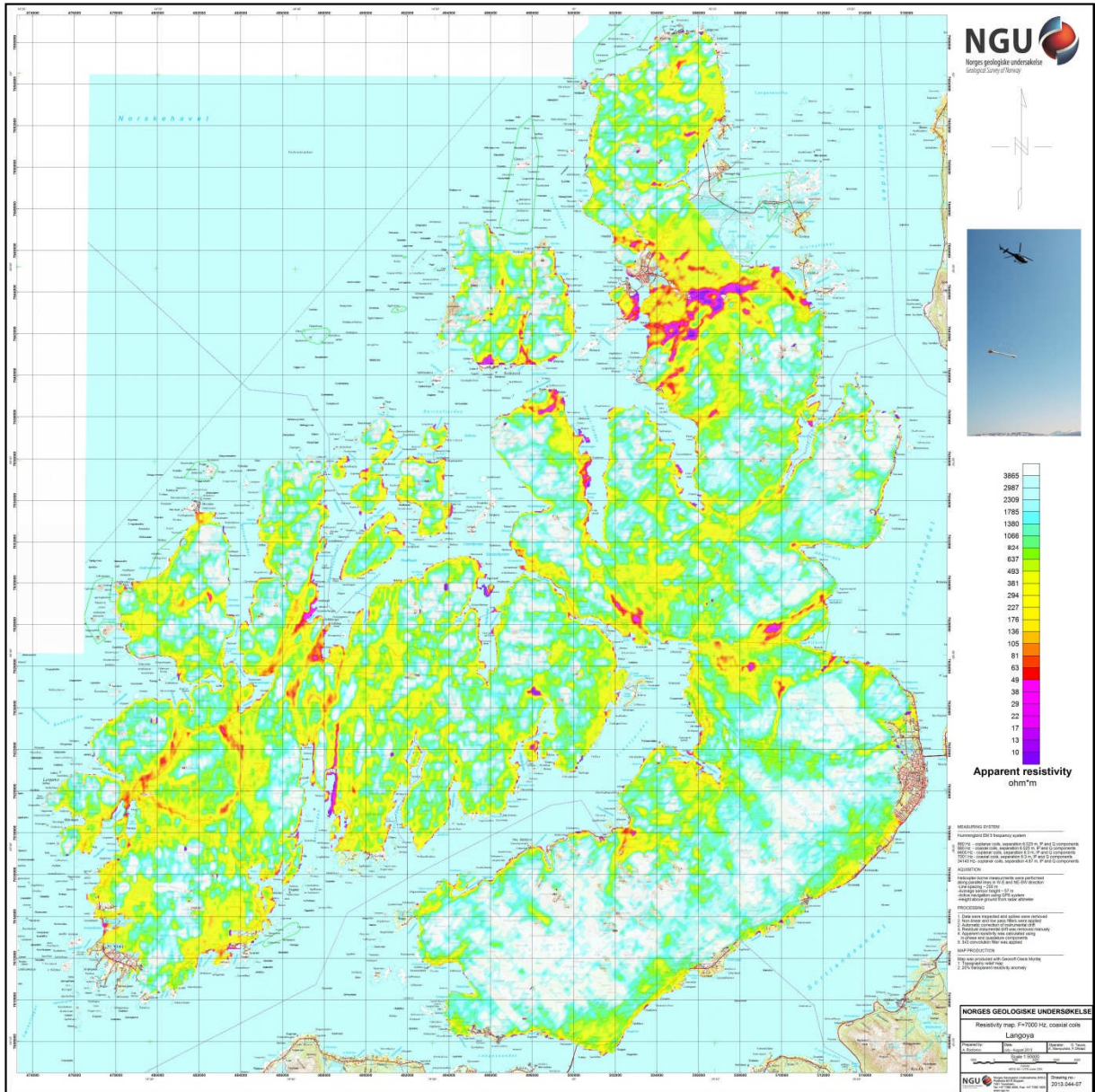


Figure 10: Apparent resistivity. Frequency 7000 Hz, Coaxial coils

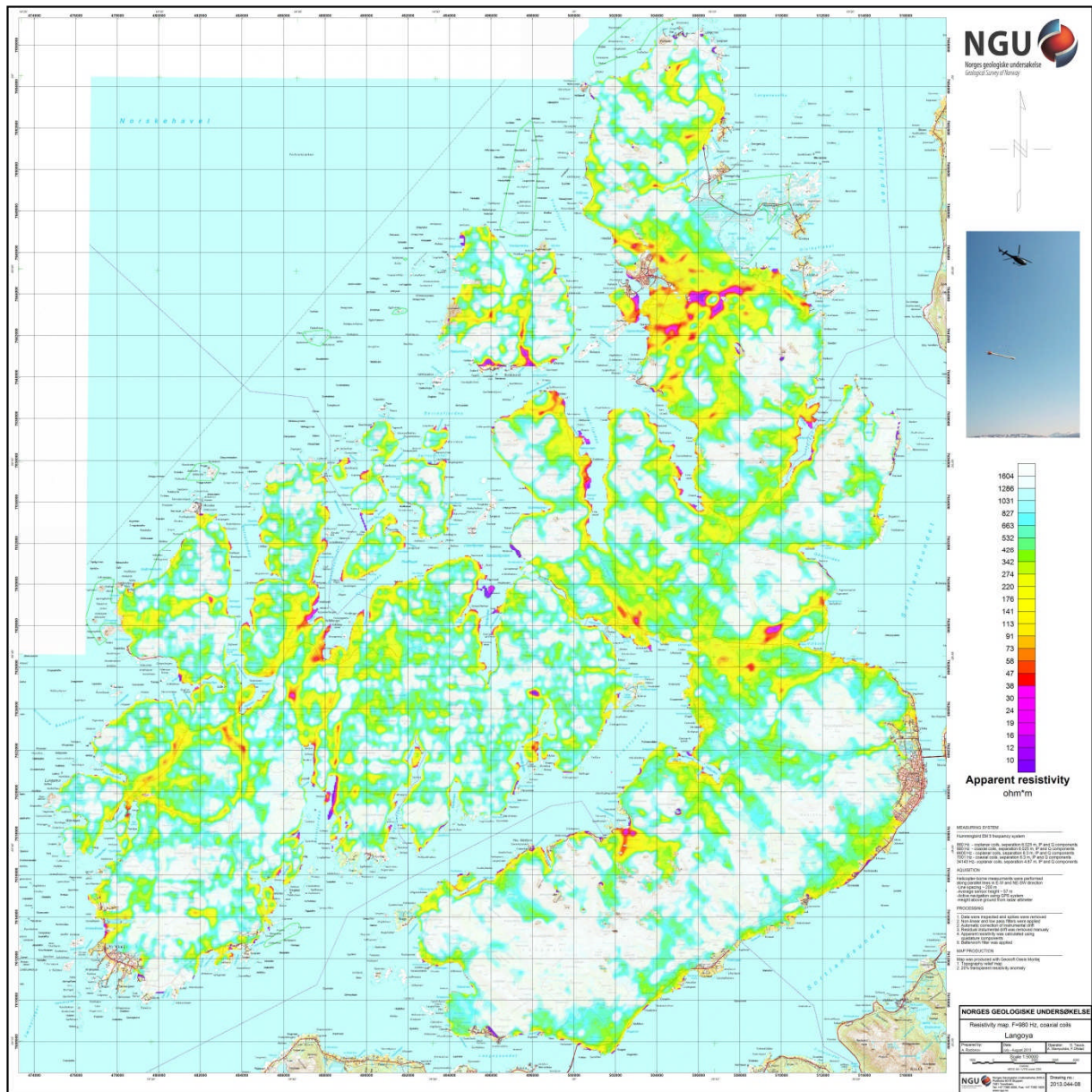


Figure 11: Apparent resistivity. Frequency 980 Hz, Coaxial coils

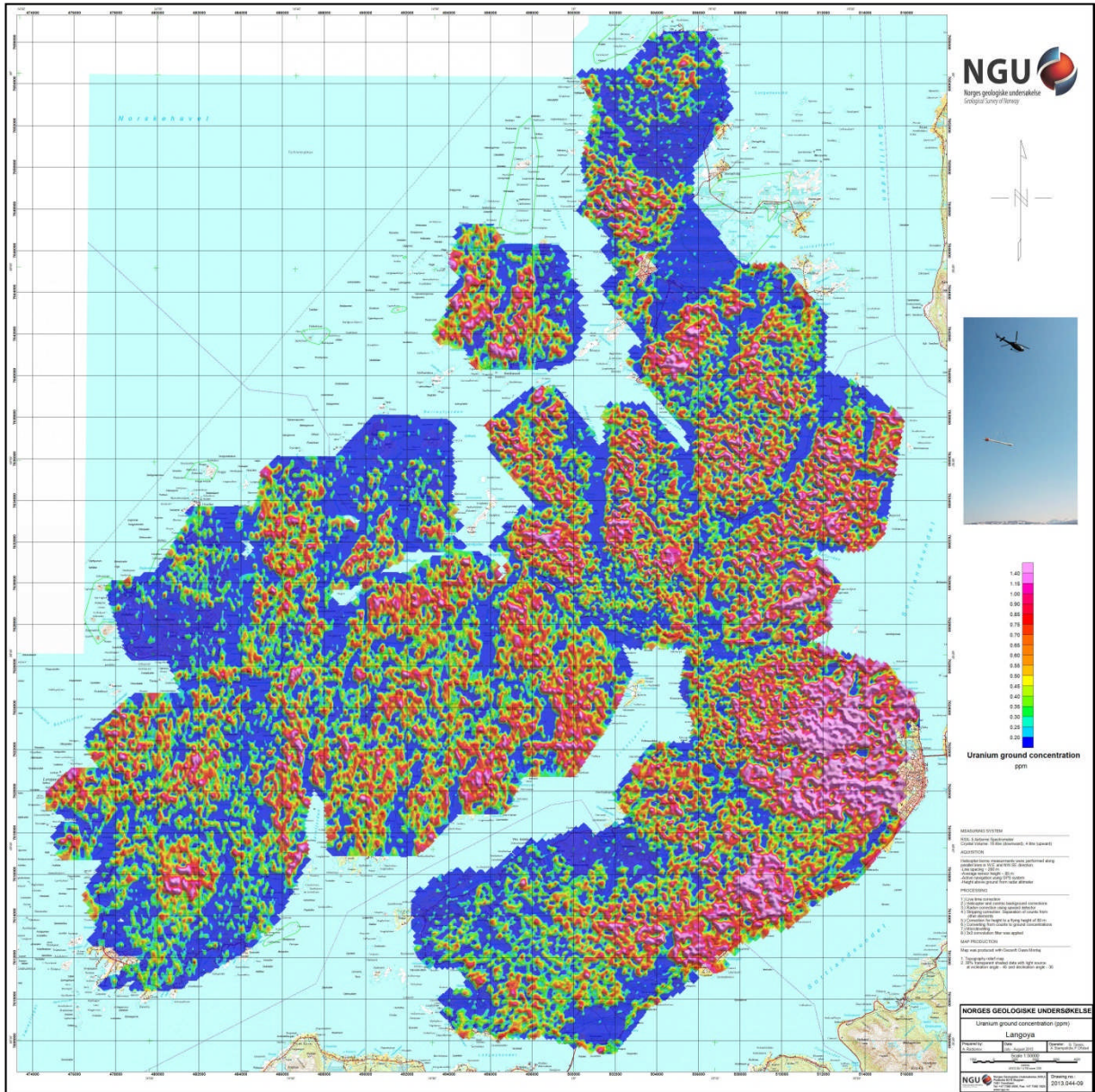


Figure 12: Uranium ground concentration

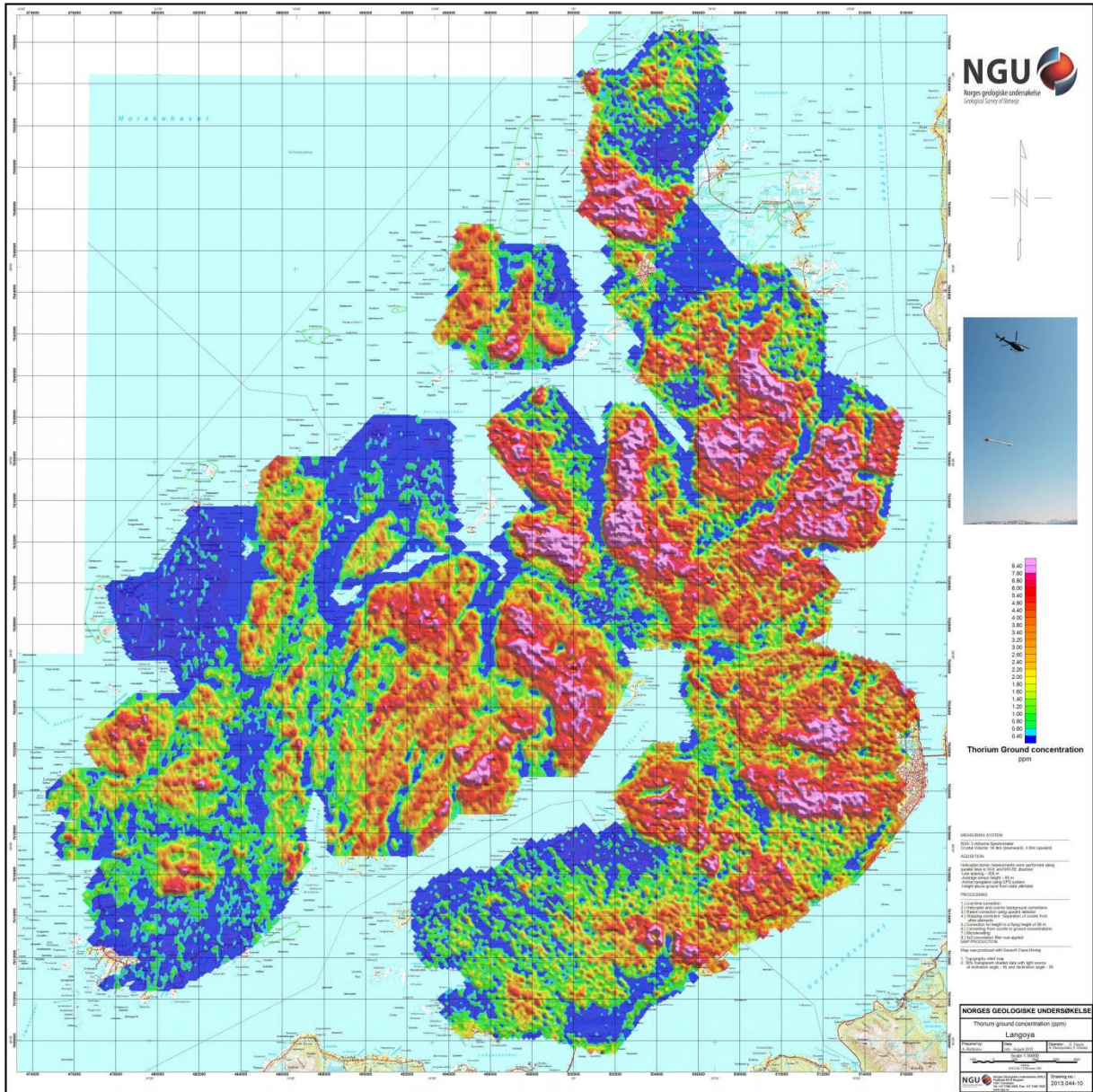


Figure 13: Thorium ground concentration

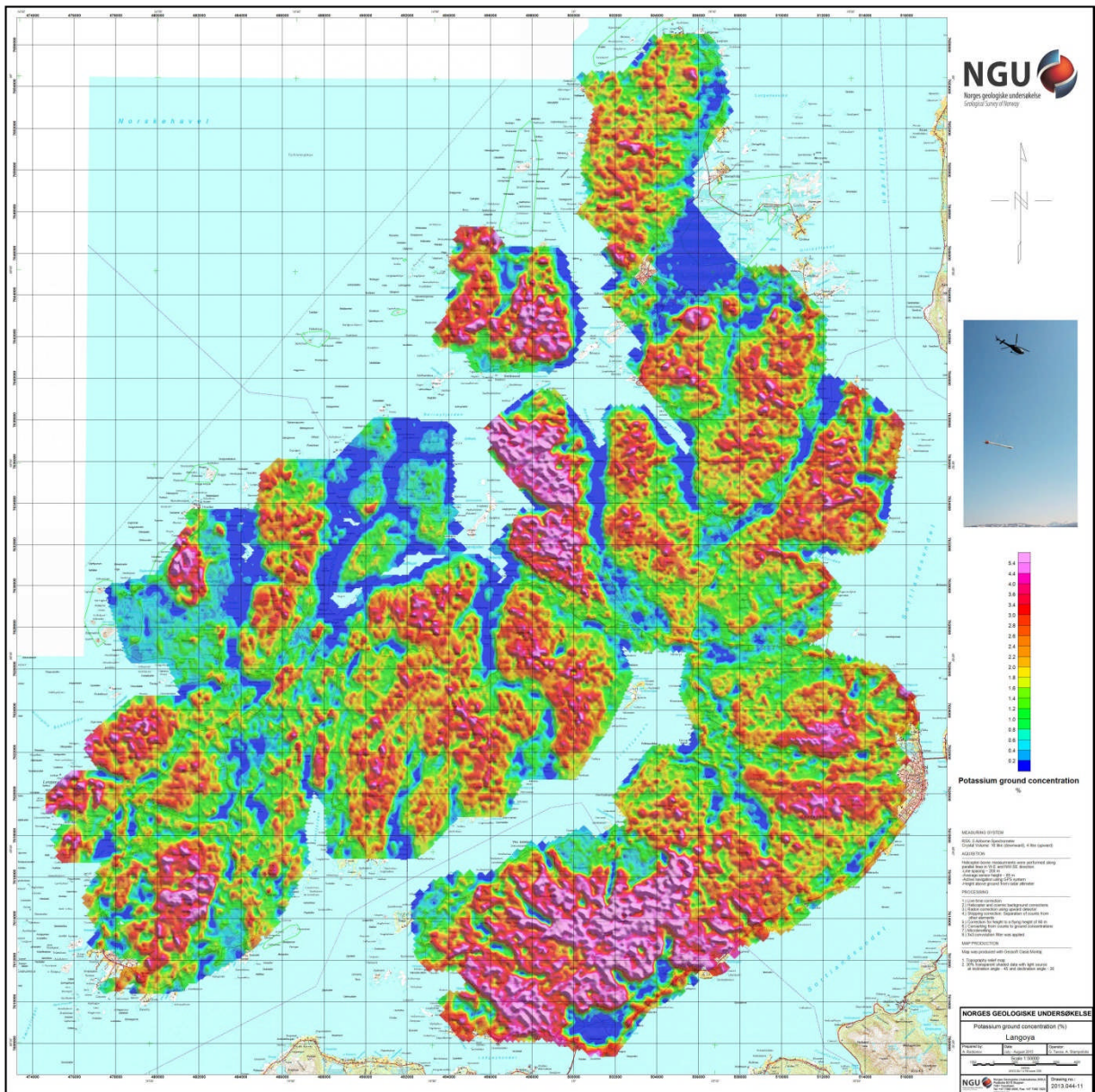


Figure 14: Potassium ground concentration

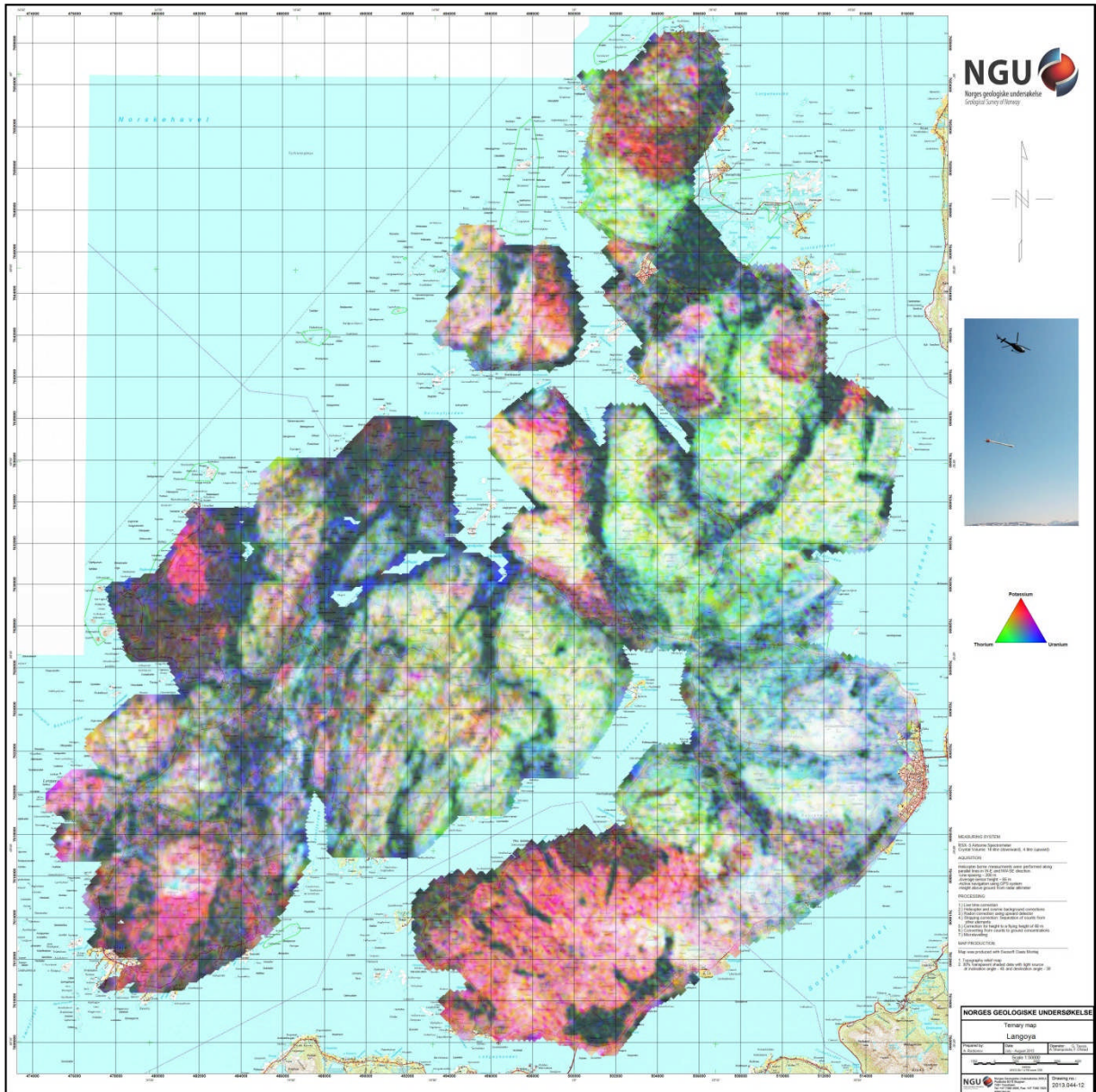


Figure 15: Radiometric Ternary map



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